

A Fast Wheel-Rail Forces Calculation Computer Code

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- Methods for the calculation of wheel-rail forces
 - Principle of proposed method
 - Comparison of proposed method with FASTSIM
 - Comparison of simulations using two different methods
 - Comparison with measurements
 - Experience with use of proposed method
 - Conclusions

Methods for Calculation of Wheel-Rail Forces



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- Exact theory by Kalker (CONTACT)
 - Simplified theory by Kalker (FASTSIM)
 - Look-up tables
 - Simple saturation functions

Methods for Calculation of Wheel-Rail Forces

Disadvantages of Common Methods



- Exact theory by Kalker (CONTACT)
 - Very long calculation time
- Simplified theory by Kalker (FASTSIM)
 - Too long calculation time in comparison with other methods

Methods for Calculation of Wheel-Rail Forces

Disadvantages of Common Methods



- Look-up tables
 - Limited data
 - Pre-calculation necessary
- Simple saturation functions
 - Spin usually not considered
 - Significant differences to the exact theory

Methods for Calculation of Wheel-Rail Forces

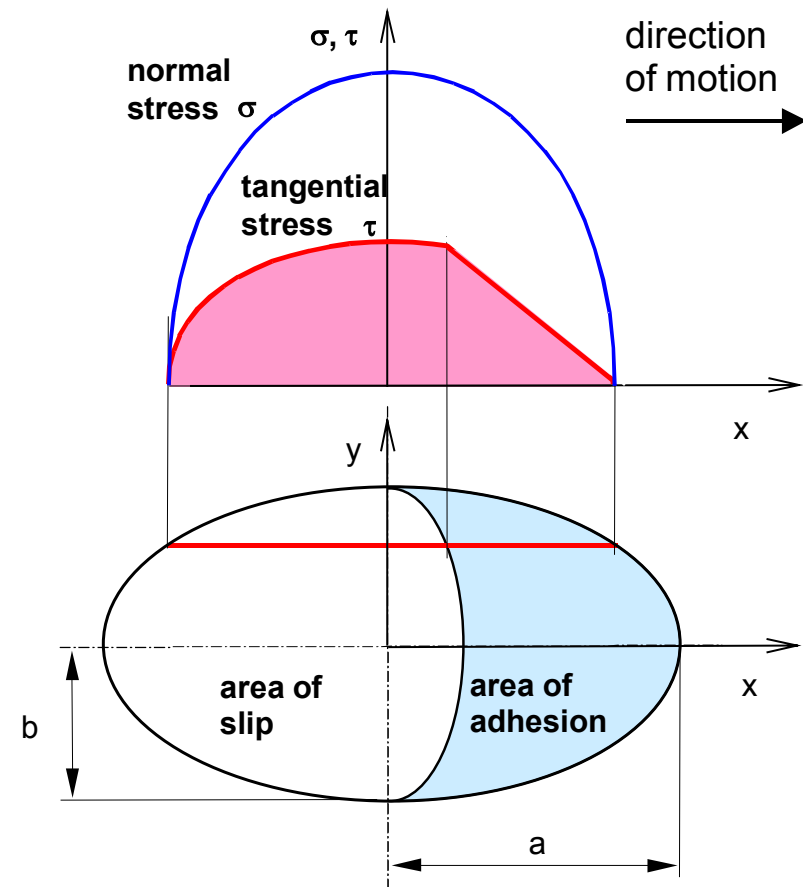
Advantages of Proposed Method



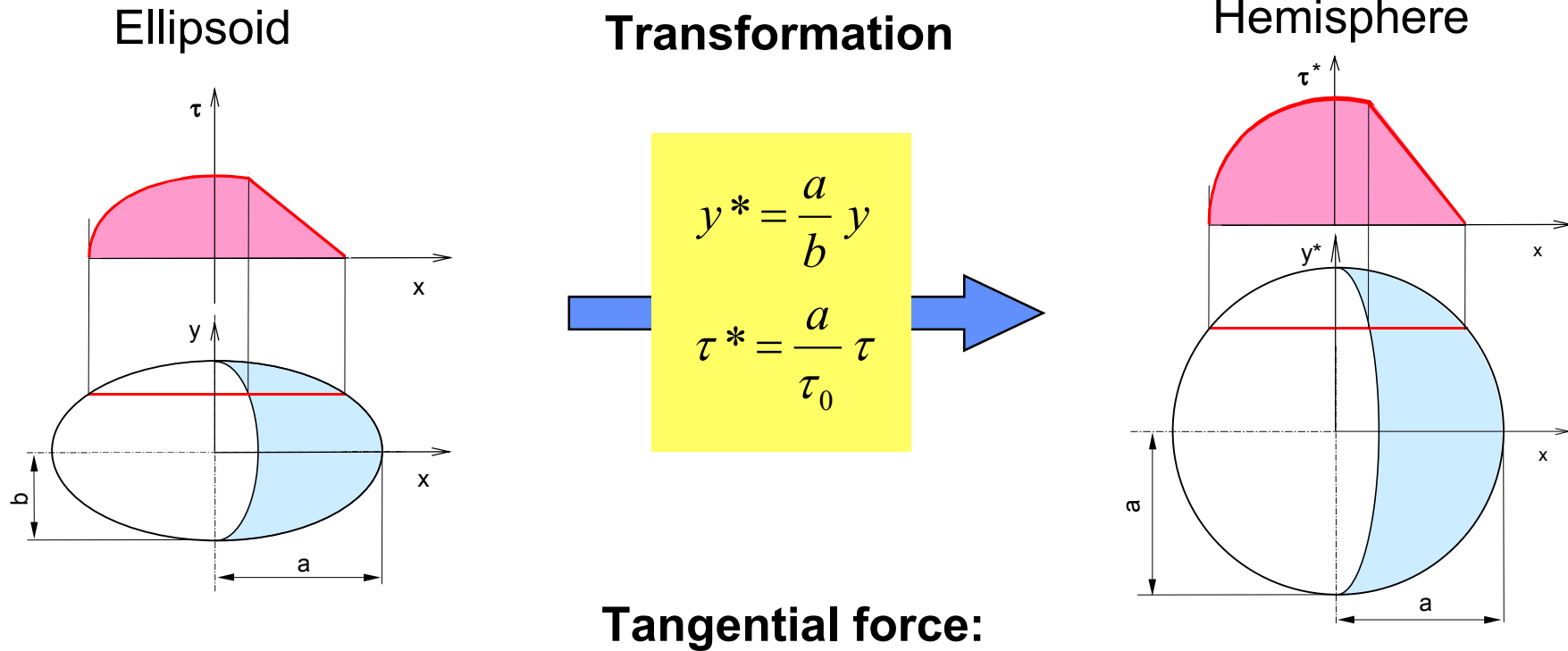
- Compromise between calculation time and necessary accuracy
- Spin taken into account
- Calculation time comparable with saturation functions or look-up tables
- Pre-calculation superfluous
- Accuracy comparable with FASTSIM or look-up tables

Principle of Proposed Method Assumptions

- Ellipsoidal contact area according to Hertz
- Coefficient of friction is constant
- Contact area is divided into area of adhesion and area of slip
- Maximal tangential stress is
$$\tau_{\max} = f \cdot \sigma$$
- Linear growth of tangential stress in area of adhesion



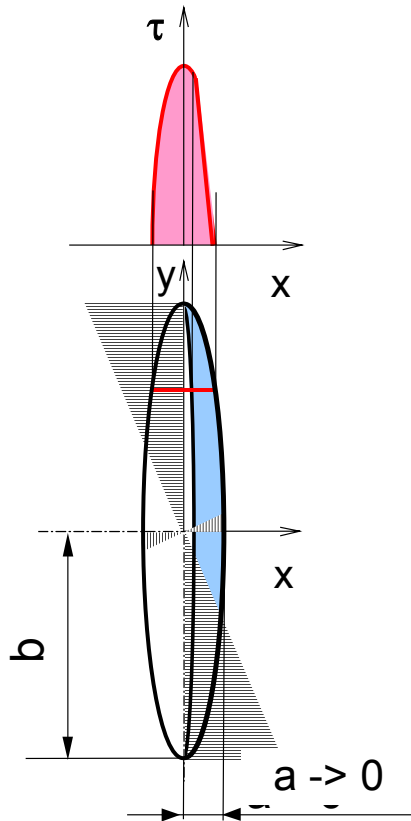
Principle of Proposed Method Transformation



$$F = \iint_{(U)} \tau \, dx \, dy = - \frac{2 \cdot Q \cdot f}{\pi} \left(\frac{\varepsilon}{1 + \varepsilon^2} + \arctan \varepsilon \right), \quad \text{where} \quad \varepsilon = \frac{2}{3} \frac{C \cdot \pi \cdot a^2 \cdot b}{Q \cdot f} s$$

Principle of Proposed Method Case of Pure Spin

$a \rightarrow 0$



Using the transformation to a hemisphere:

$$F_y = -\frac{3}{8} \pi \cdot \tau_0 \cdot a \cdot b \left[|\varepsilon| \left(\frac{\delta^3}{3} - \frac{\delta^2}{2} + \frac{1}{6} \right) - \frac{1}{3} \sqrt{(1 - \delta^2)^3} \right]$$

$$\text{where } \delta = \frac{\varepsilon^2 - 1}{\varepsilon^2 + 1}$$

Principle of Proposed Method

Use of the Proposed Method



- On the basis of experiment

Constant C given by comparison with experiment

- As a fast solution with the constants from Kalker

$$C = \frac{3}{8} \frac{G}{a} c_{jj} \quad \text{where} \quad c_{jj} = \sqrt{\left(c_{11} \frac{s_x}{s} \right)^2 + \left(c_{22} \frac{s_y}{s} \right)^2}$$

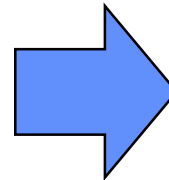
$$C_s = \frac{4}{\pi} \frac{G \cdot \sqrt{b}}{\sqrt{a^3}} c_{23}$$

Principle of Proposed Method

Full Solution: Programme ADH

INPUT :

- Wheel load
- Coefficient of friction
- Modulus of rigidity
- Semiaxis of contact ellipse
- Kalker's constants
- Longitudinal and lateral creep
- Spin



OUTPUT :

- Longitudinal force
- Lateral force

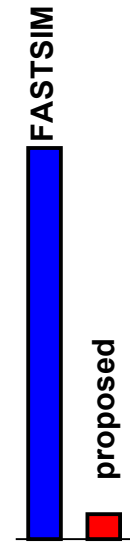
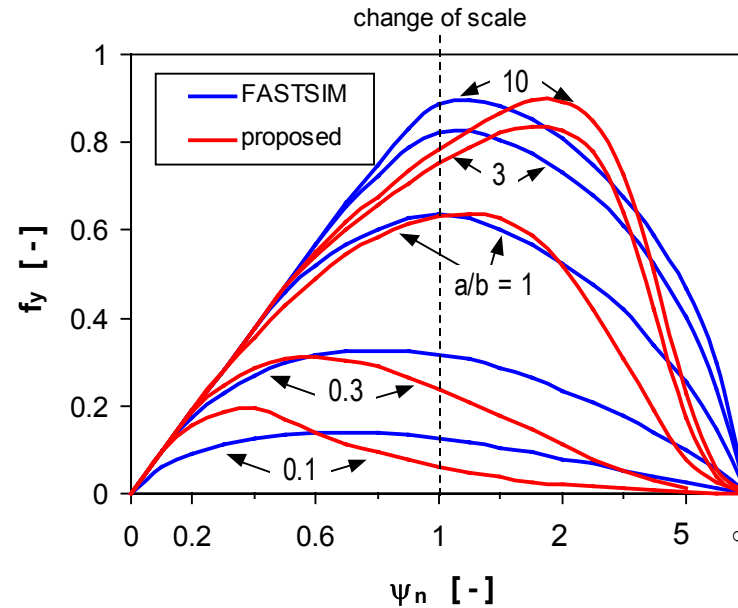
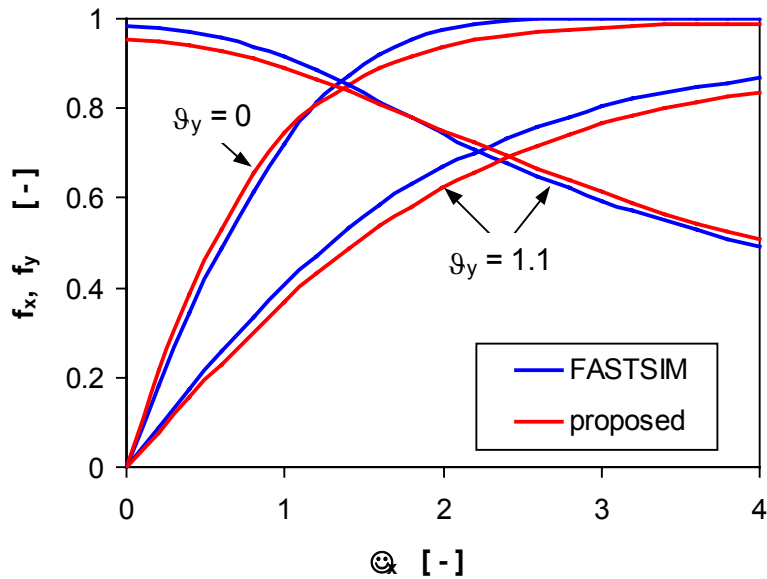
Comparison with Programme FASTSIM



longitudinal and lateral creep

pure spin

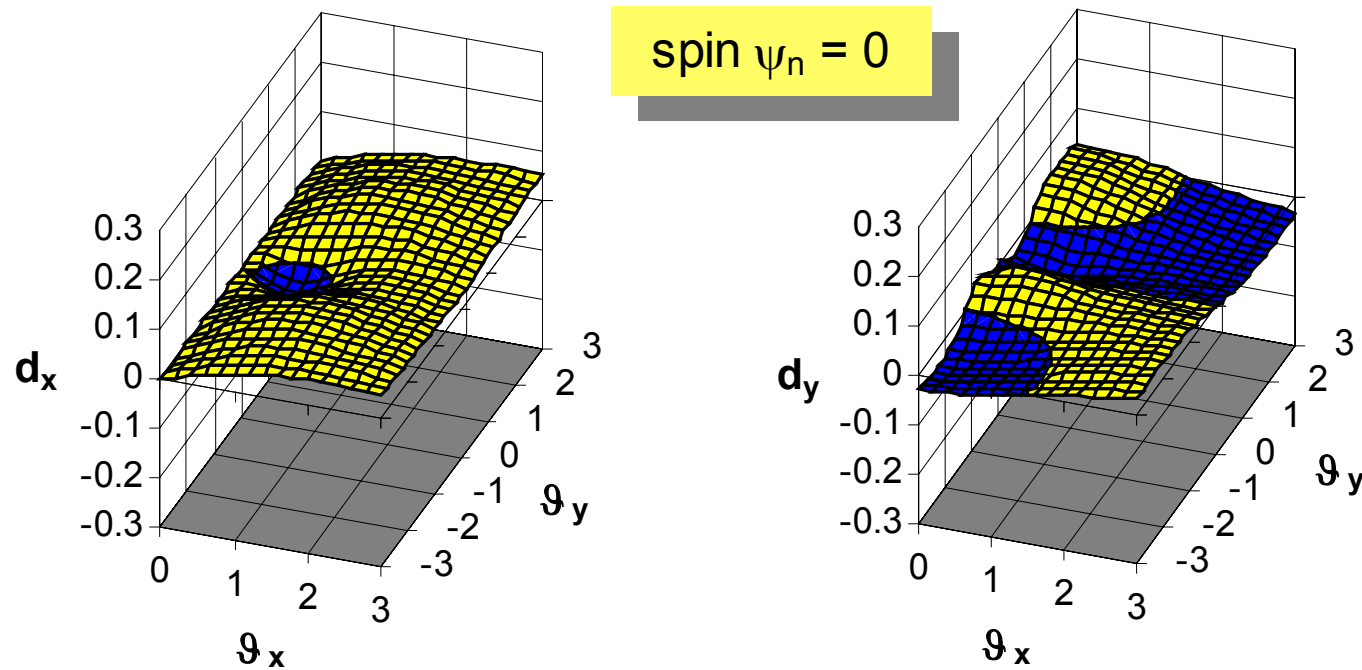
calculation time



Comparison with Programme FASTSIM

Difference between the two methods:

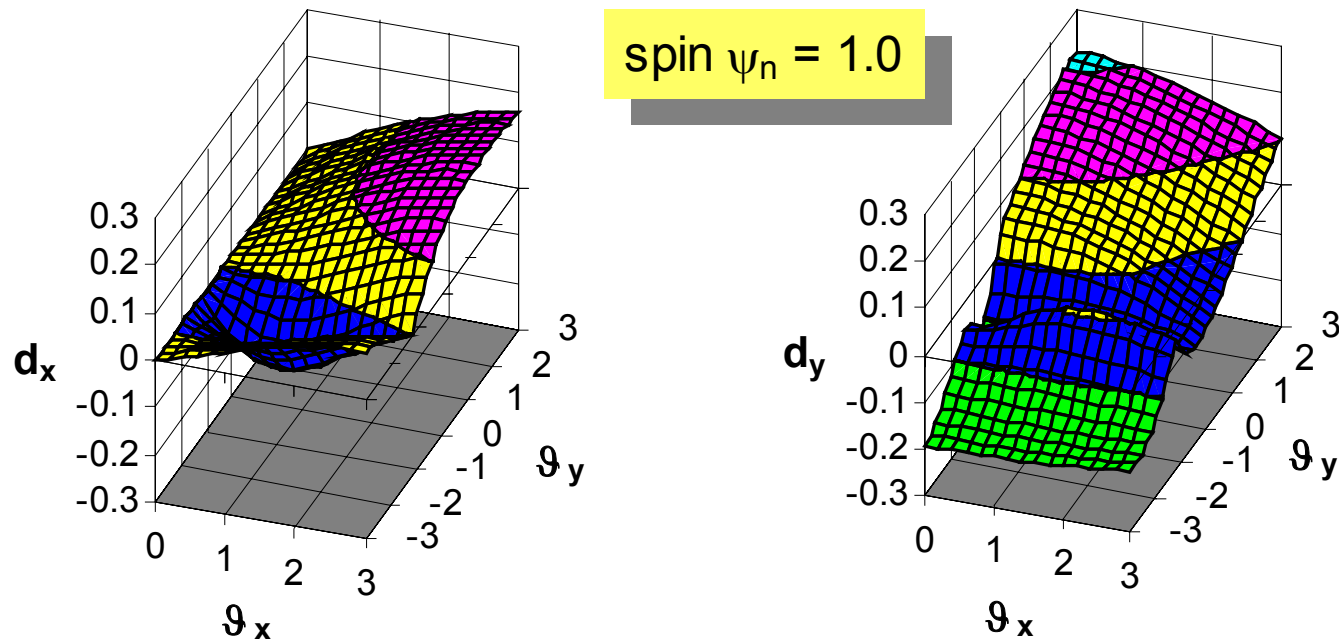
$$d_i = f_{iK} - f_{iP} \quad i = x, y$$



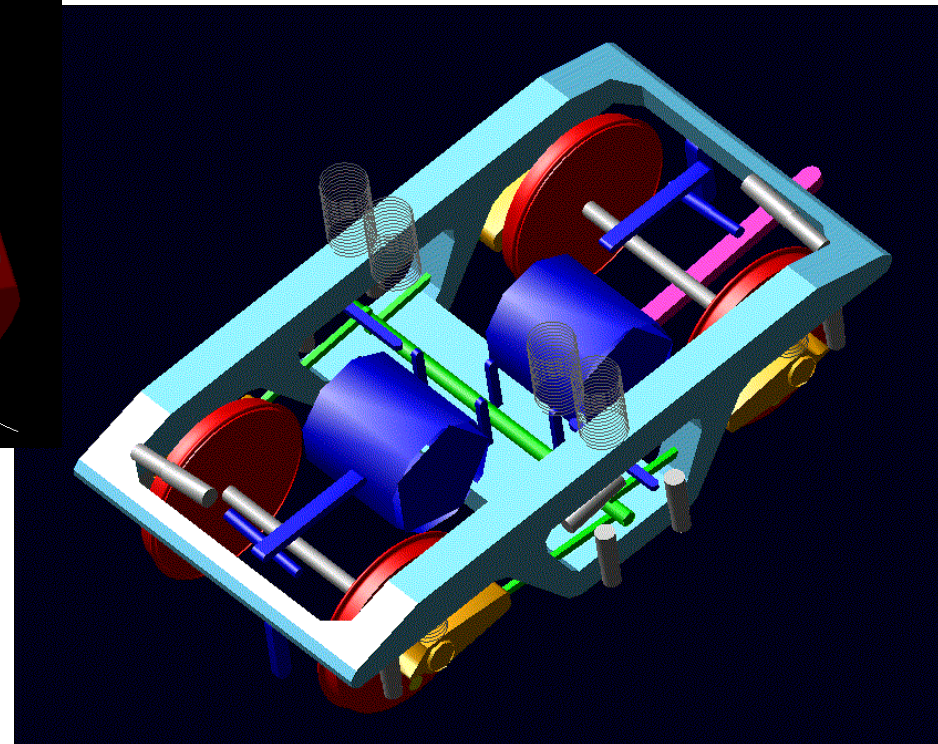
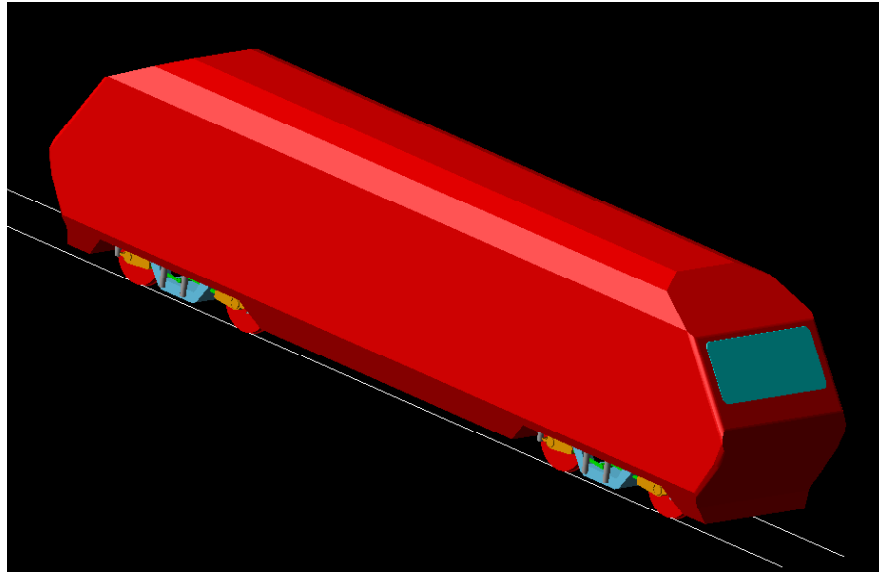
Comparison with Programme FASTSIM

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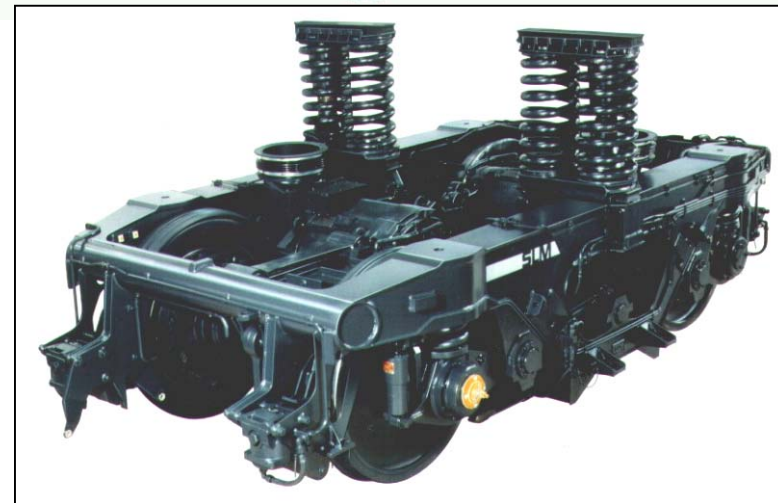
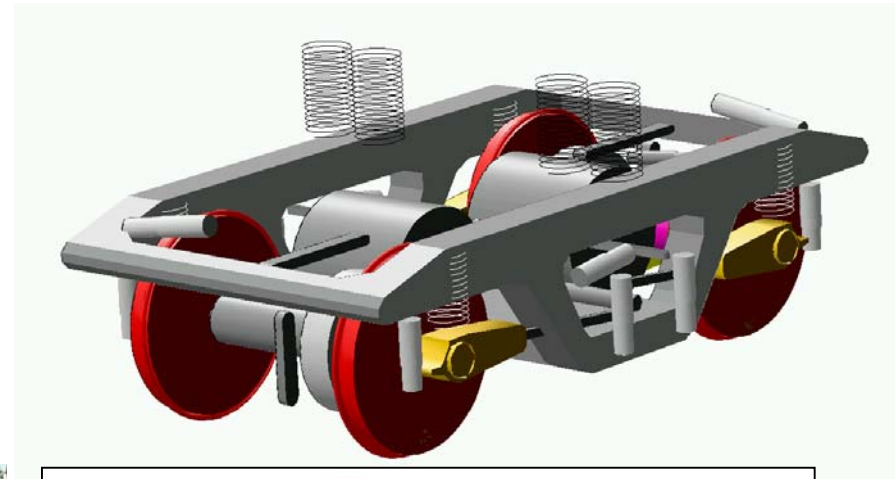
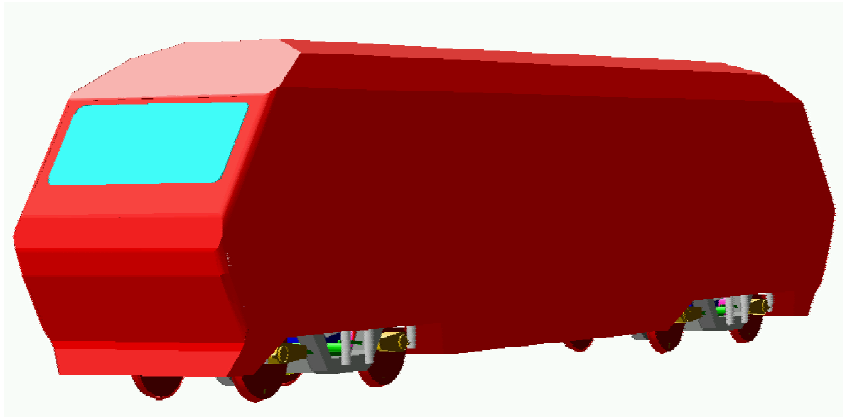


Comparison of Simulations ADAMS/Rail Model

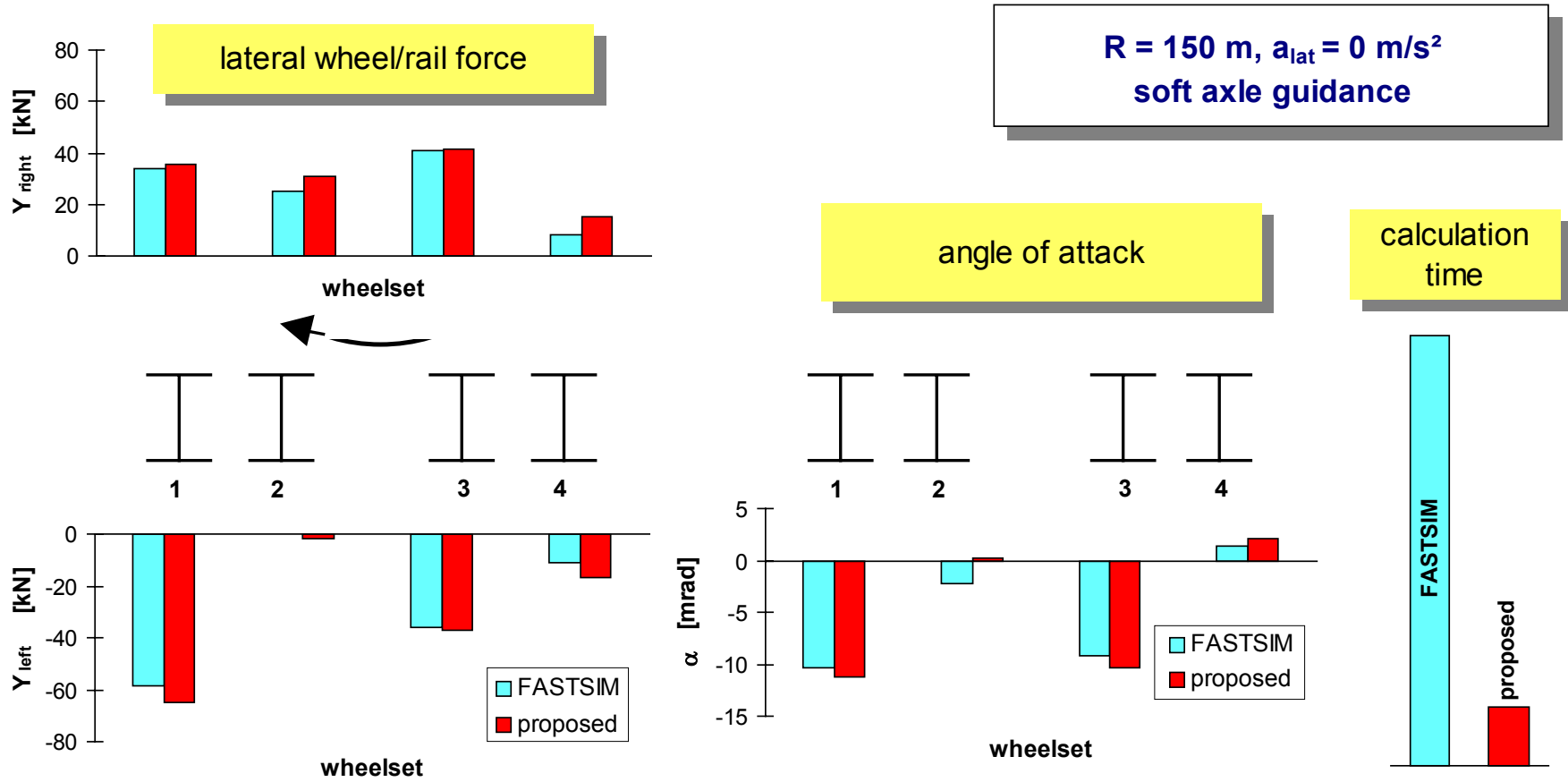


- 51 rigid bodies
- 84 bushings
- 4 bump-stops
- 24 dampers

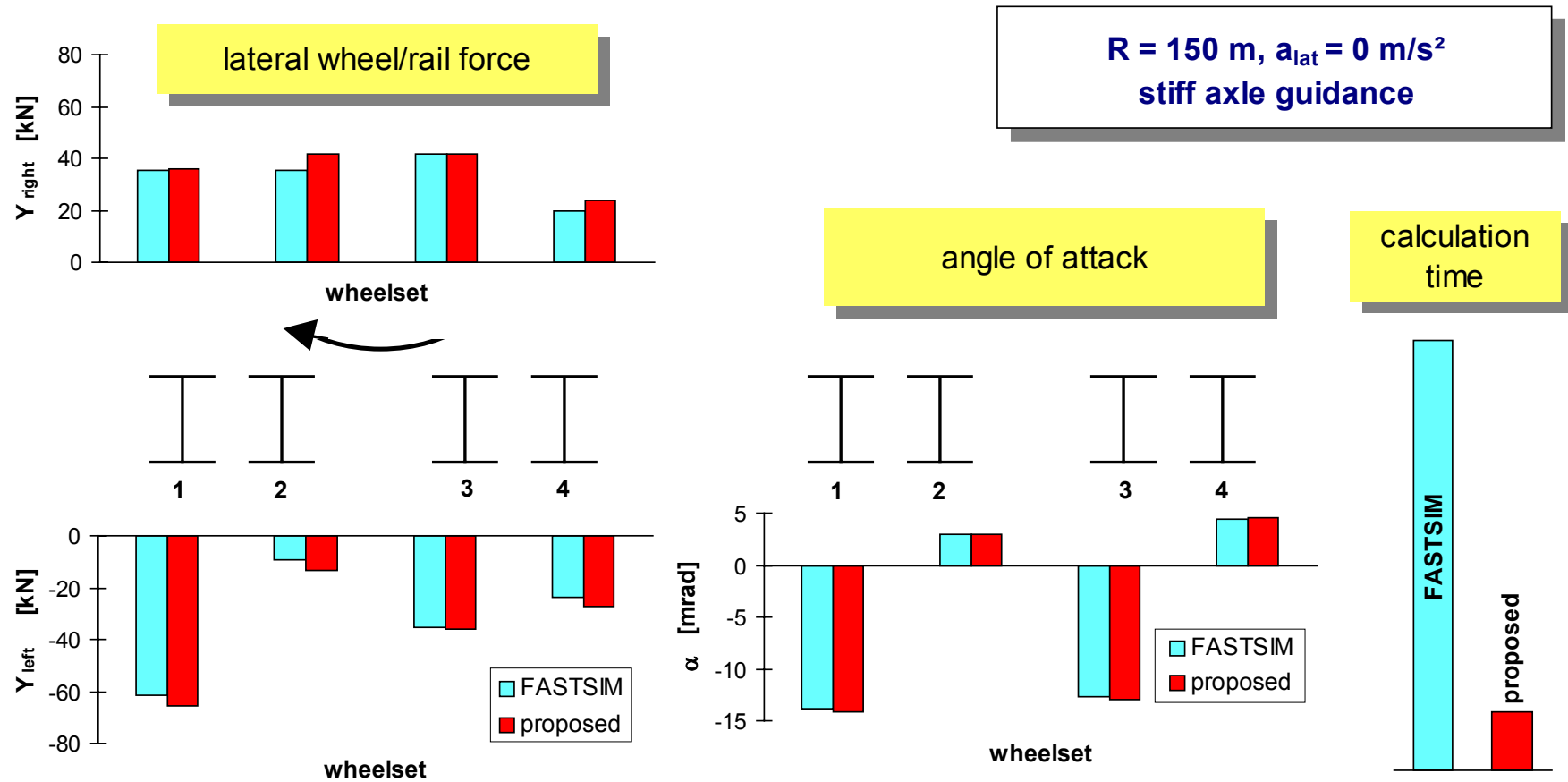
Comparison of Simulations ADAMS/Rail Model



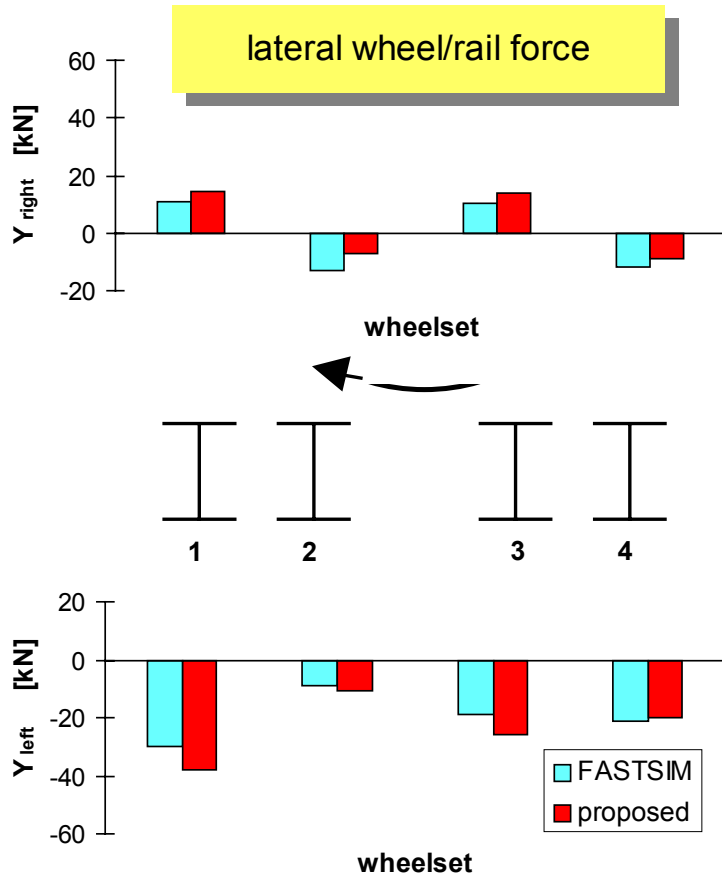
Comparison of Simulations Use of FASTSIM and of Proposed Method



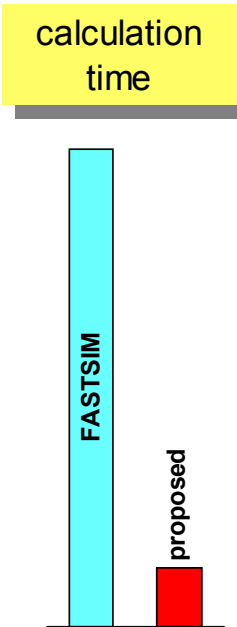
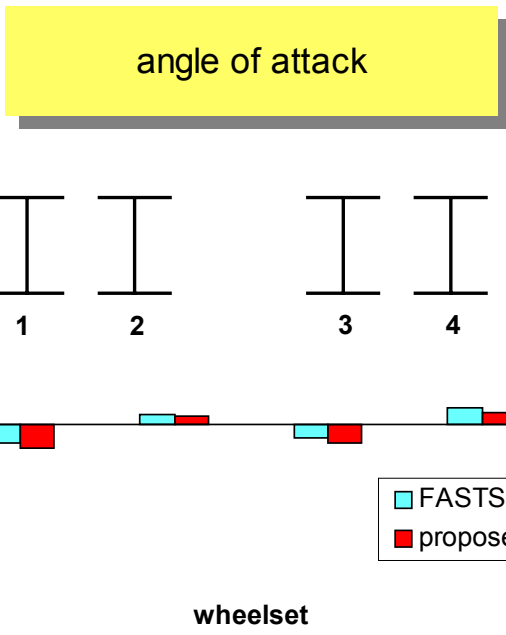
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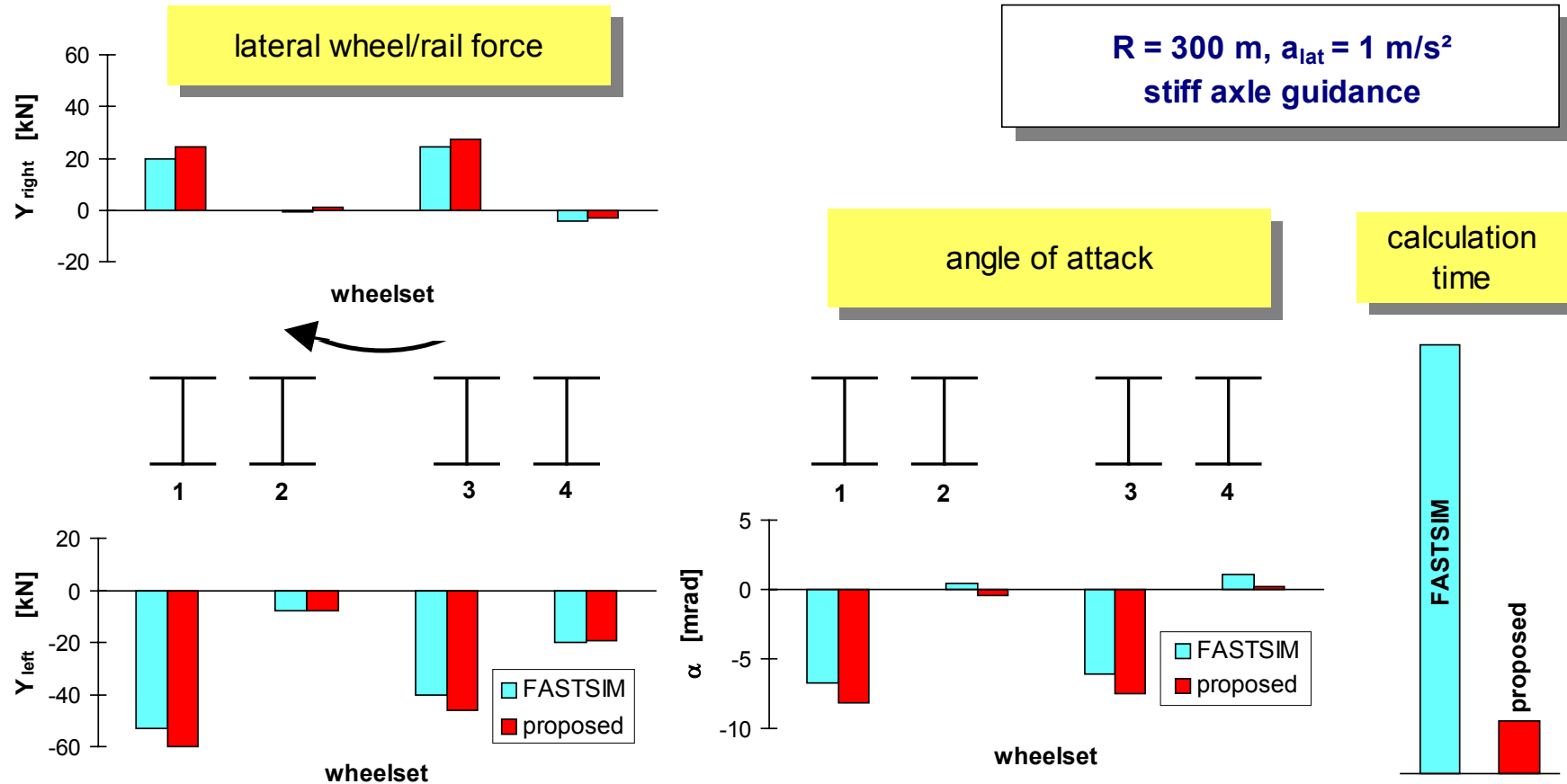
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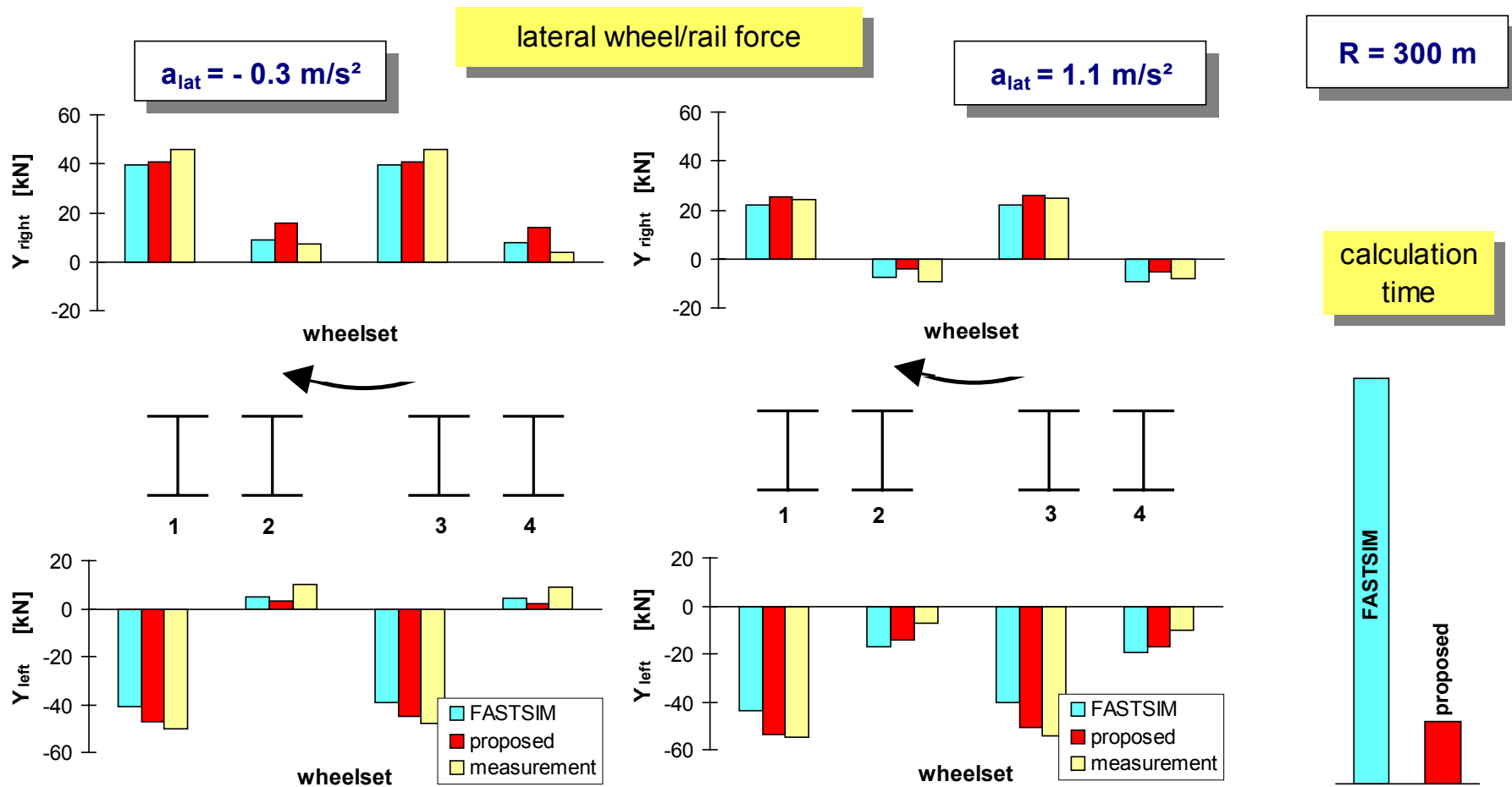
R = 300 m, a_{lat} = 1 m/s²
soft axle guidance



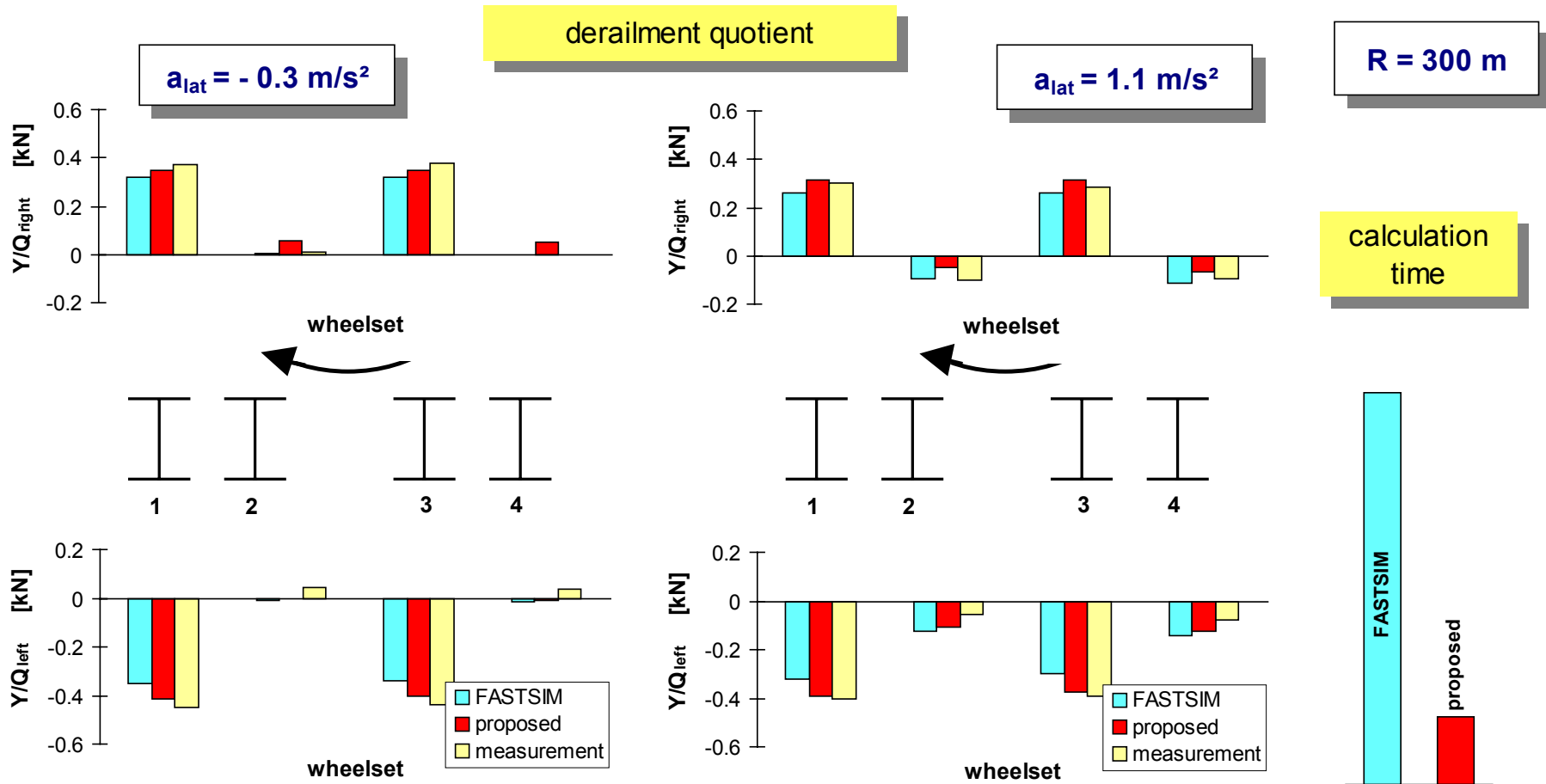
Comparison of Simulations Use of FASTSIM and of Proposed Method



Comparison with Measurements



Comparison with Measurements



Experience with Use of Proposed Method



- Algorithm in use in different programmes since 1990
- Positive experience in research as well as in industrial application
- Standard method in the programme ADAMS/Rail
- Tested and possible for use as user routine in programmes: SIMPACK, MEDYNA, GENSYS, SIMFA

Proposed method

- Is a fast alternative to Kalker's method
- Allows calculations of full non-linear wheel-rail forces
- Takes spin into account
- Makes saving of pre-calculated values superfluous
- Shows good agreement in comparison with measurements
- Has been used in different simulation tools with very good experience